

## Research Paper


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# A new compact and wideband CPW-fed sleeve antenna

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## Abstract

In this article, a sleeve antenna with a wide impedance bandwidth that consists of a coplanar waveguide line connected to a metallic cylinder is presented. The effect of design parameters on the impedance bandwidth is considered by some simulations. In addition to the wide impedance bandwidth, the omnidirectional pattern, high efficiency, low cost and easy fabrication process, and compact dimensions cause this antenna to be a good choice for some applications at low VHF/UHF frequency bands. Due to the flexible structure of this antenna, it is possible to cover the various frequency bands by changing the parameters of the antenna. In this work a typical model of the proposed antenna for the frequency range of 127 to 586 MHz is fabricated and compared with other previous works. An equivalent circuit model has been proposed to better understand how the antenna works. The proposed antenna has a bandwidth of about 128.7% for a voltage standing wave ratio (VSWR) of less than 3, compact size of  $0.274\lambda \times 0.047\lambda$  and higher than 90% efficiency.

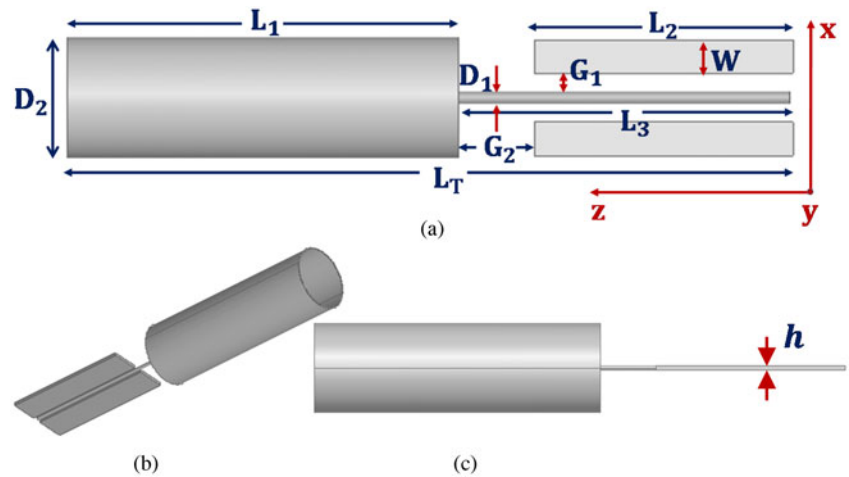
## Introduction

Nowadays wideband antennas are being used in many applications in order to guarantee higher data transmission rates. Therefore, the bandwidth increment is one of the most important characteristics in the antenna design which has been taken into consideration during recent years. In addition, attention must be paid to the compact size and low fabrication cost as the other prerequisites for the design of the wideband antennas. Till now, several methods have been introduced for designing the wideband antennas, from which, one can point out to the sleeve usage in the monopole antennas. Since the sleeve antenna has all of the mentioned features, it is used in a large number of wideband purposes.

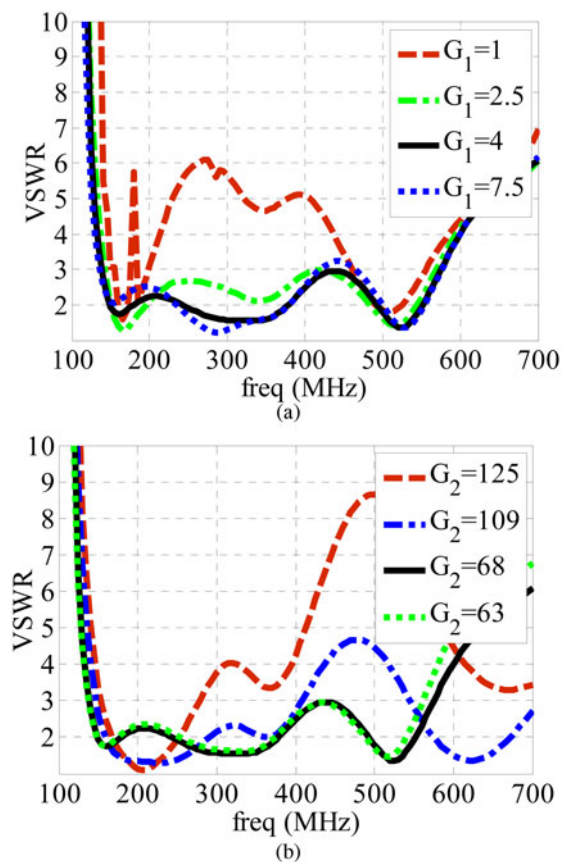
For example, an end loaded dual sleeve antenna with a bandwidth of 127.3% for voltage standing wave ratio (VSWR)  $< 3$  is introduced in [1]. The size of this antenna is about  $0.35\lambda \times 0.075\lambda$ . In another study, the bandwidth of 123.1% has been obtained with the dimension of  $0.35\lambda \times 0.07\lambda$  and the same VSWR by using a sleeve dipole antenna with a tuneable plate element at the end of that [2]. In addition, several other investigations are available dealing with the usage of the printed structures for designing the sleeve wideband antennas [3–11]. An important consideration in the design of the wideband antennas is the compromise between the increasing bandwidth and shrinking antenna's dimensions. Generally, in most of the previous studies, the antenna's dimensions have been inevitably increased in order to increase the bandwidth. This challenge can be further seen in the case of very high frequency (VHF)/ultra-high frequency (UHF) low frequency wideband antennas. The innovation in this work is the new structure of the proposed antenna, which use the coplanar waveguide (CPW) feeding as a sleeve to overcome the challenge of the bandwidth and size and also to implement the planar sleeve. In this case we have more design parameters to match the input impedance in various frequencies.

In this paper, the design challenge of the wideband antennas within the low frequency range is investigated and improved by providing a new plan. The effect of the main parameters of the proposed plan on improving the antenna's performance is evaluated through conducting various simulations. Also, the equivalent circuit model presented for the observed series and parallel resonance behavior. Finally, the proposed antenna design, while being of small dimension, can provide a wide range of impedance bandwidths in the range of VHF/UHF frequencies. In addition to the expressed features, the present proposed antenna has an omnidirectional pattern which increases its usage in the cases such as the jamming systems.

The paper's framework is constructed as in the following. In 'Antenna design and simulation results', the general structure of the antenna and important parameters in its design are introduced. In this section, by presenting the simulation results, the effect of the design parameters is examined on the basic features of the antenna such as the impedance bandwidth. An equivalent circuit model has been proposed to better understand how the antenna has multiple resonance behavior. In 'Experimental verifications and antenna comparison', the obtained results of the bandwidth measurements are given along with fabricating the antenna prototype.



**Fig. 1.** CPW-fed sleeve antenna structure composed of a CPW feed line connected to a metal cylinder as the main radiating element: (a) top view, (b) 3D view, and (c) side view.

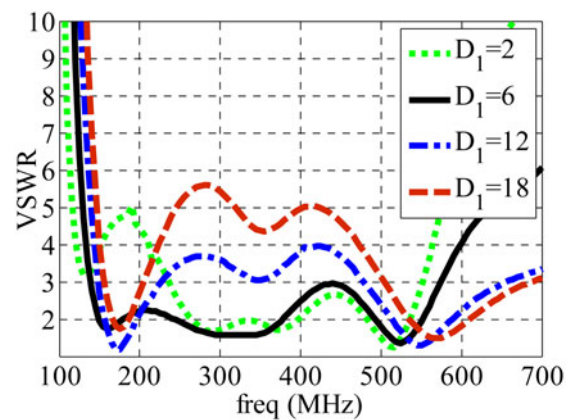


**Fig. 2.** Simulated VSWR characteristic for various values of (a)  $G_1$  and (b)  $G_2$ .

Then, a comparison of the proposed antenna with the other introduced ones in the previous investigations is given in this section in a tabular format. Ultimately, the conclusion will be presented in 'Conclusion'.

### Antenna design and simulation results

The structure of the proposed antenna and corresponding geometric parameters are shown in Fig. 1. As depicted by Fig. 1,



**Fig. 3.** Simulated VSWR characteristic for various values of  $D_1$ .

the antenna is composed of a CPW feed line connected to a metal cylinder as the main radiating element.

The most important design parameters of this antenna include the gap between the line and ground plane in the CPW feed section specified by  $G_1$  and the one between the antenna's feed section and cylindrical radiating element which has been shown by  $G_2$ . The other design parameters are illustrated in Fig. 1.

In the following, the influence of these parameters on the antenna's impedance bandwidth is investigated through conducting several simulations. All of the simulated results have been obtained using the high frequency structure simulator (HFSS) software which is based upon the finite element method.

It should be said that the bandwidth evaluation criteria for all of the presented results is  $VSWR < 3$ . Using several simulations, Fig. 2 illustrates the effect of changes in the values of  $G_1$  and  $G_2$  on the antenna impedance bandwidth. The simulation results indicate that  $G_1$  which controls the characteristic impedance of the CPW transmission line, affects the matching rate (VSWR value) over the whole antenna's bandwidth. On the other hand,  $G_2$  can control the impedance bandwidth of the antenna in the higher edge frequency, so that the bandwidth starting frequency is not affected.

The effect of changes in the  $D_1$  parameter is shown in Fig. 3. Similar to  $G_1$ , this parameter can also change the characteristic impedance of the CPW transmission line and adjust the matching

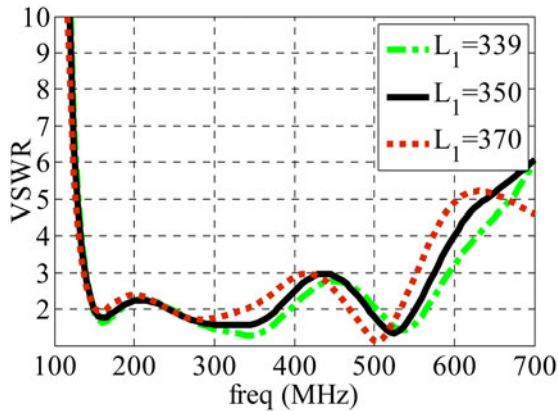


Fig. 4. Simulated VSWR characteristic for various values of  $L_1$ .

Table 1. Optimum dimension of the proposed antenna

Dimensions	(mm)	Dimensions	(mm)
$L_1$	350	$G_2$	68
$L_2$	231.2	$D_1$	6
$L_3$	296.2	$D_2$	110
$L_T$	646.2	$W$	45.5
$G_1$	4	$h$	5

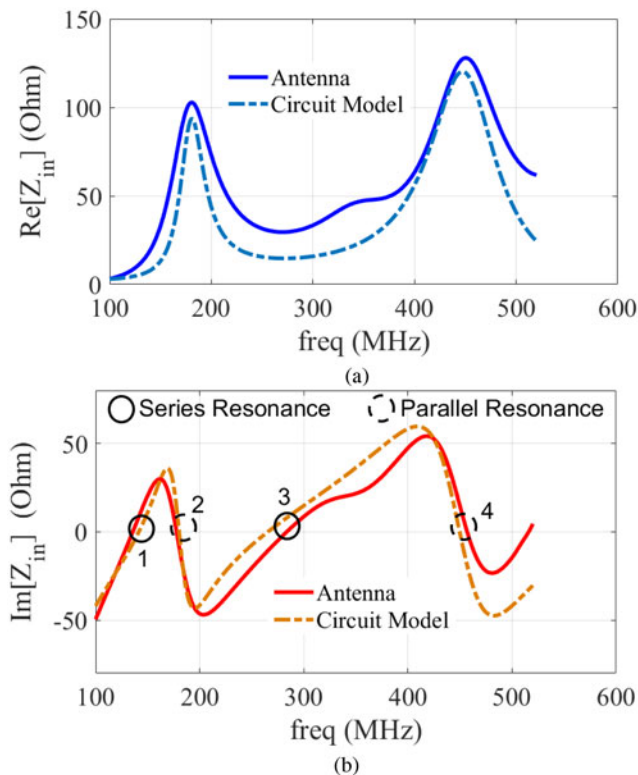


Fig. 5. Comparison of the input impedance of the antenna with the equivalent circuits model: (a) real part and (b) imaginary part.

rate. In fact, with increasing and decreasing  $D_1$ , the capacitive and inductive property of the CPW transmission line is changed which yields the impedance matching variation, as a consequence.

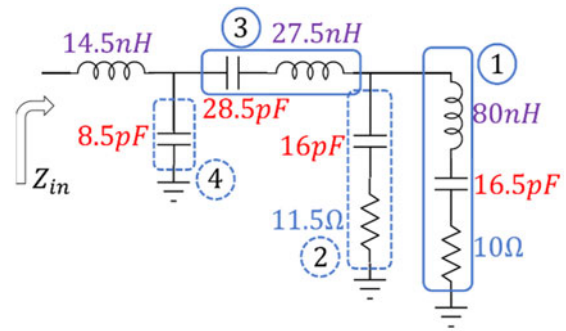


Fig. 6. Equivalent circuits model of the antenna.

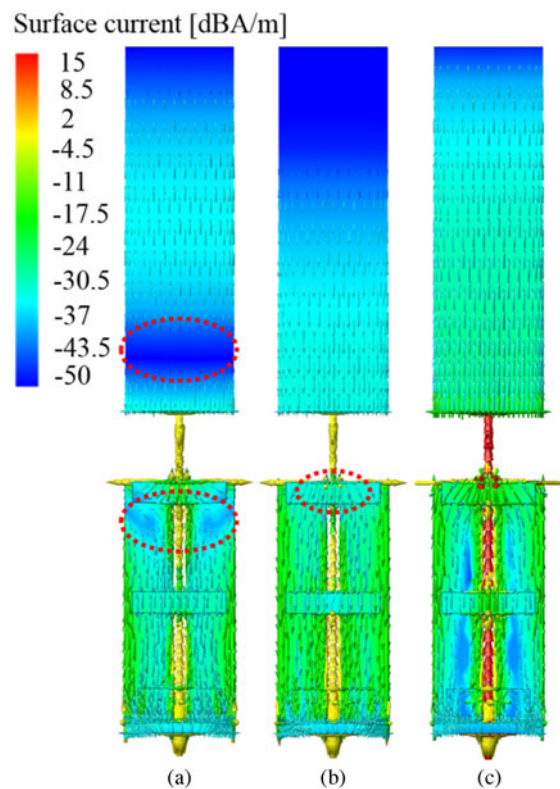
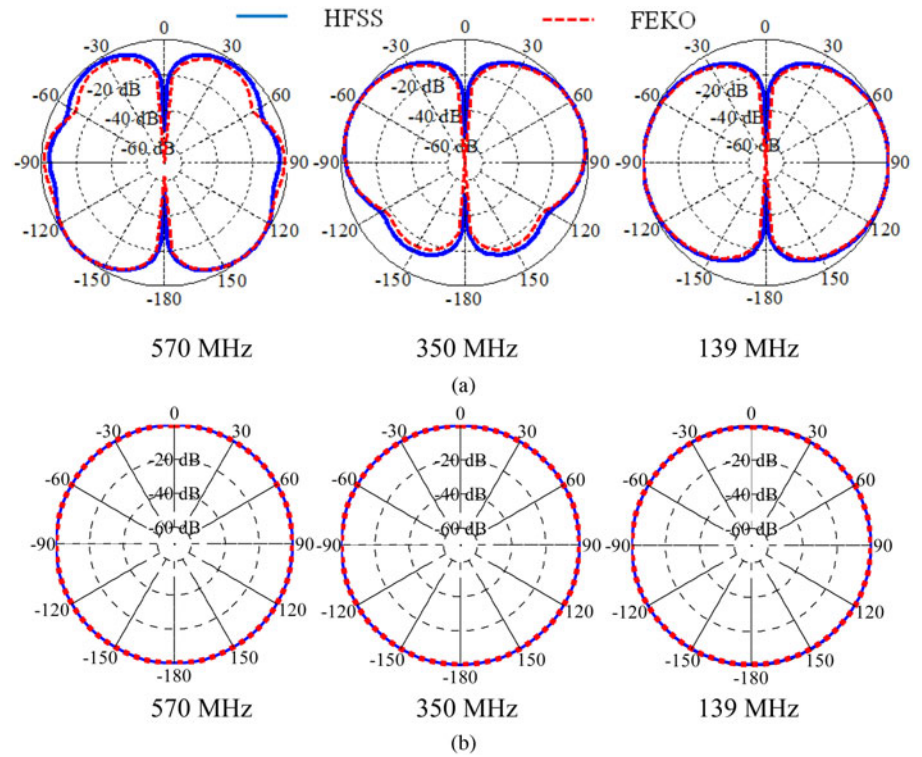


Fig. 7. Current distribution on the proposed antenna: (a) 570, (b) 350, and (c) 139 MHz.

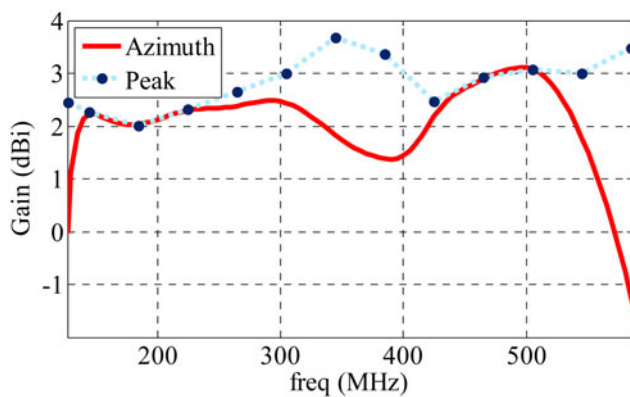
Figure 4 represents the impedance bandwidth variation with changes in  $L_1$ . Simulations illustrate that  $L_1$  basically affects the higher edge frequency, so that the matching frequency decreases at the end of the band as  $L_1$  increases. This parameter has no significant effect on the matching of the antenna.

It is noteworthy that in all the simulations performed for the different values of the above parameters, the overall length of the  $L_T$  antenna is constant. In other words, the bandwidth increase of this antenna has not been accompanied by the antenna length increment. Generally, the overall dimension of the antenna which is a function of the two parameters of  $L_T$  and  $D_2$ , solely specifies the beginning frequency of the antenna's impedance bandwidth.

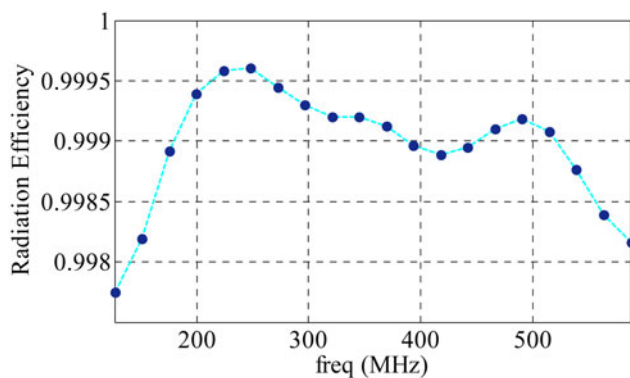
In all of the performed simulations in Figs 2–4, when the effect of each of the four parameters is investigated, the other three are considered to be constant. For example, when  $G_1$  is considered,



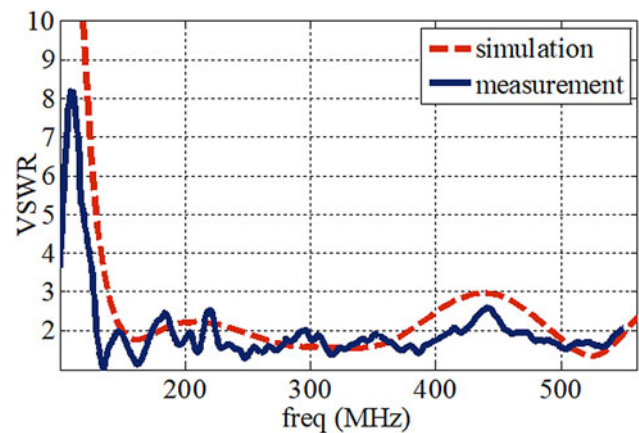
**Fig. 8.** Radiation patterns of  $E_{\theta}$ -component: (a)  $E$ -plane and (b)  $H$ -plane.



**Fig. 9.** The azimuth and peak gain of the proposed antenna.



**Fig. 10.** Radiation efficiency of the proposed antenna.



**Fig. 11.** Measured and simulated VSWR for the proposed antenna.

$G_2$ ,  $D_1$ , and  $L_2$  must be kept constant. The other design parameters of the antenna in Fig. 1 such as  $L_2$ ,  $W$ , and  $L_3$  are functions of the four main parameters ( $L_1$ ,  $D_1$ ,  $G_1$ , and  $G_2$ ). By increasing  $D_1$ ,  $W$  must be reduced due to the parameters such as  $G_1$  and  $D_2$  which have been considered to be constant. After performing the above simulations, the optimized dimensions of the antenna are given in Table 1.

After obtaining the antenna optimum design parameters, it simulated and the input impedance of the antenna has been achieved. The real and the imaginary parts of the input impedance illustrated in Fig. 5. The imaginary part of the input impedance shows that the antenna in the operation bandwidth has four resonances i.e. two series and two parallel resonances (see Fig. 5(b)). The simple equivalent circuit model for simple dipole antenna consists of series RLC [resistor (R), inductor (L), capacitor (C)]

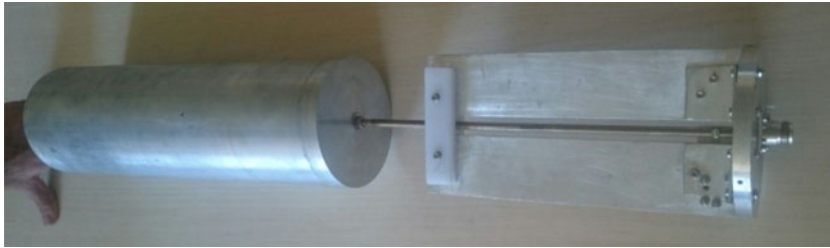


Fig. 12. Photograph of the proposed antenna.

Table 2. Comparison with other antennas

Reference antenna	Frequency range (GHz)	BW (%)	Dimension ( $L \times w$ )
[1]	0.7 – 3.15	127.3	$0.35\lambda \times 0.075\lambda$
[2]	1 – 4.2	123.1	$0.35\lambda \times 0.07\lambda$
[3]	2.1 – 3.7	55.2	$0.44\lambda \times 0.29\lambda$
[4]	0.44 – 1.35	101.7	$0.615\lambda \times 0.134\lambda$
[5]	1.35 – 4.85	112.9	$0.519\lambda \times 0.127\lambda$
[6]	0.65 – 2.85	125.7	$0.452\lambda \times 0.318\lambda$
[7]	3 – 13	125	$0.524\lambda \times 0.419\lambda$
[8]	2.8 – 12	124.3	$0.391\lambda \times 0.391\lambda$
[9]	2.15 – 4.5	70.7	$0.586\lambda \times 0.586\lambda$
[10]	2.8 – 11.3	120.57	$0.644\lambda \times 0.435\lambda$
This Work	0.127 – 0.586	128.7	$0.274\lambda \times 0.047\lambda$

elements and the first resonance is due to it. It is shown in Fig. 6 in part one. The other part added in sequence to create the next resonances (see Fig. 6). The value of the inductor and the capacitor computed based on the resonance frequency and the resistances control the peak value in the real part. The comparison of the antenna input impedance and the equivalent circuit model is illustrated in Fig. 5 and shows good agreement.

Figure 7 shows the simulated surface current of the antenna at 139, 350, and 570 MHz respectively. It is clear that by increasing the operation frequency, the current phase changes along the antenna length. As shown in figure, there is one and two current phase changing at 350 and 570 MHz respectively. As we know, the number of radiation pattern lobes begins to increase due to the current phase changing which has been shown in Fig. 8(a).

Figure 8 shows the radiation pattern of the simulated antenna in  $E$  and  $H$ -planes and for three different frequency values. The radiation pattern has been simulated by the FEKO simulator to validate the HFSS simulator result. As would be observed from this figure, it is clear that the proposed antenna has the same pattern as a monopole one in the  $E$ -plane and also the pattern is omnidirectional in the  $H$ -plane.

The variation of the maximum and azimuth antenna gain is plotted in Fig. 9 over the frequency. As can be seen, the gain is positive at all covered frequency bandwidth and the maximum gain is about 3.68 dBi at 0.345 GHz.

Figure 10 shows the variation of the radiation efficiency over the frequency. The figure indicates that the antenna has a high efficiency that promising around 99%.

## Experimental verifications and antenna comparison

In order to validate the simulation results, an antenna prototype is fabricated according to the dimensions given in Table 1. Figure 11 represents the results obtained via the simulation and measurement of the fabricated antenna. As can be seen from this figure, good agreement has been achieved and indicates  $VSWR < 3$  for this antenna within the frequency range of 127–586 MHz. Figure 12 shows the schematic view of the fabricated antenna.

Table 2 gives a comparison of the proposed antenna with that introduced by previous research studies from the dimensions and impedance bandwidth point of views. Regarding the items mentioned in this table, the proposed antenna dimensions are smaller in size compared to the dimensions of the similar antennas with a similar impedance bandwidth.

## Conclusion

The novel wideband CPW-fed sleeve antenna was numerically and practically investigated and due to its flexible structure, all of the antenna's parameters were tuned to achieve a bandwidth of about 129% for a VSWR of less than 3, compact size of  $0.274\lambda \times 0.047\lambda$ , and higher than 90% radiation efficiency. In this regard, the simulation results were shown based on the parameters tuning and the reason for each of the effects explained as well. The omnidirectional behavior of the antenna pattern has also been shown in three frequencies over the bandwidth. Eventually, the agreement was observed between the measurement and simulation results and the comparison was also made with the other works. As a result, this antenna provided the three main features including the high bandwidth, compact size, and omnidirectional pattern therefore, it could be used for any application which needs all of these in a simultaneous manner.

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